

Worldwide Pollution Control Association

Duke Energy Seminar
September 3 – 5, 2008
Concord, NC



Visit our website at www.wpca.info

A large, vertical arrangement of the letters "W", "P", "C", and "A" in a bold, blue, sans-serif font. The letters are positioned over a grayscale image of a globe, which shows the continents of North and South America. The letters have a slight drop shadow, giving them a three-dimensional appearance as if they are floating above the globe.



WAHLCO, INC.[®]

Flue Gas Conditioning

WPCA

September 3, 2008

William Hankins

VP Sales

Outline

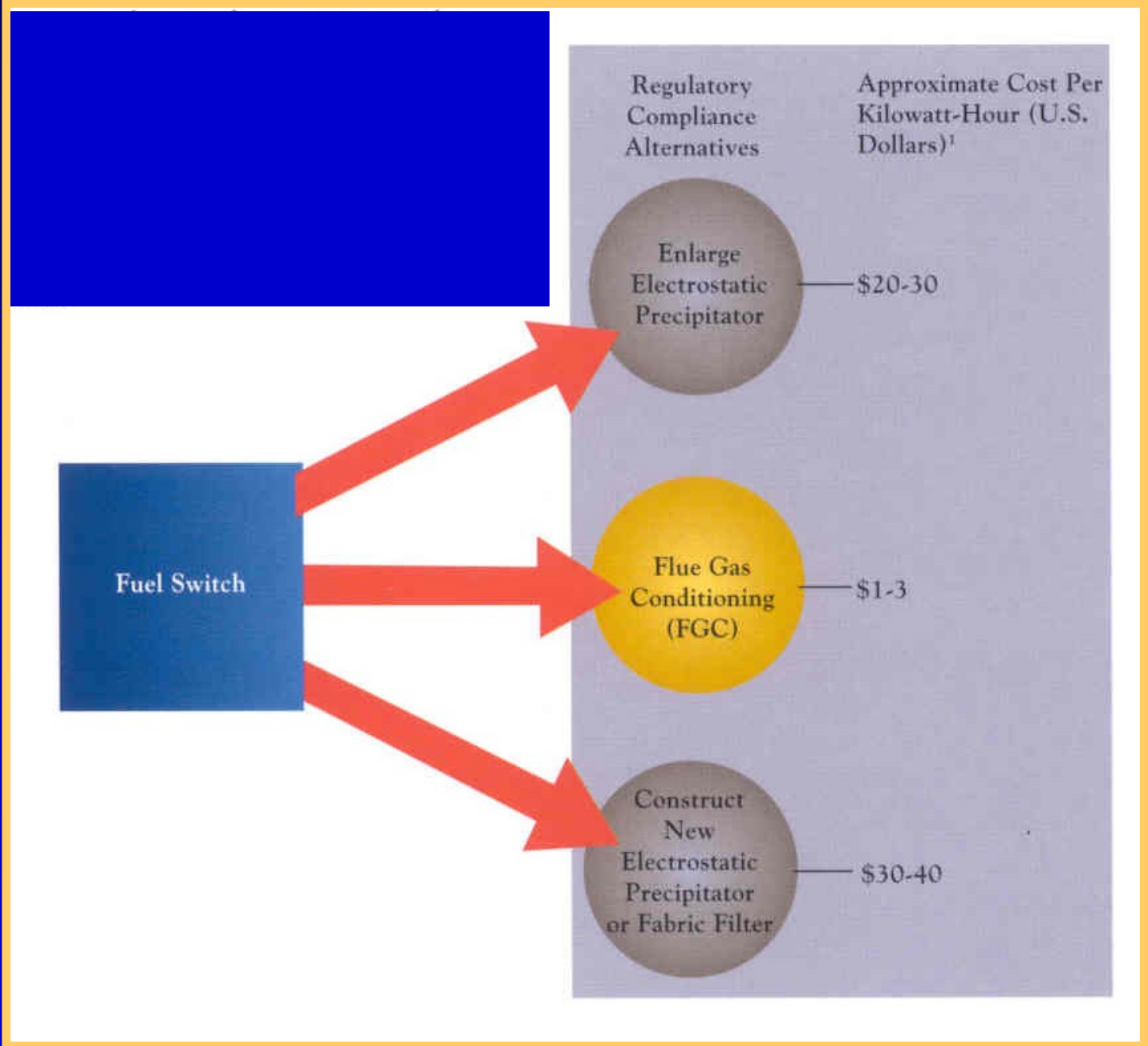
- What is SO₃ FGC
- Electrostatic Precipitation Fundamentals
- Ash Resistivity
- SO₃ Process
- Design Principles



SO₃ FGC Background

- Sulfur Trioxide Flue Gas Conditioning
- Corrects Ash Resistivity to Improve performance of Electrostatic Precipitators (ESPs)
- Small amount injected upstream of ESP
- Approximately 1500 units worldwide
- Commercialized by Wahlco in early 1970's





Sulfur Emissions

Typical Sulfur Oxide Emissions from Coal-Burning Boilers

Sulfur Oxides PPMV		3.5% Sulfur Content	0.5% Sulfur Content	0.5% Sulfur & FGC
Entering Precipitator	SO ₂	2600	370	371
	SO ₃	26	4	10
Entering Stack	SO ₂	2600	370	375
	SO ₃	7	4	4

Flue gas conditioning does not increase emission levels of sulfur oxides (SO₂ or SO₃).

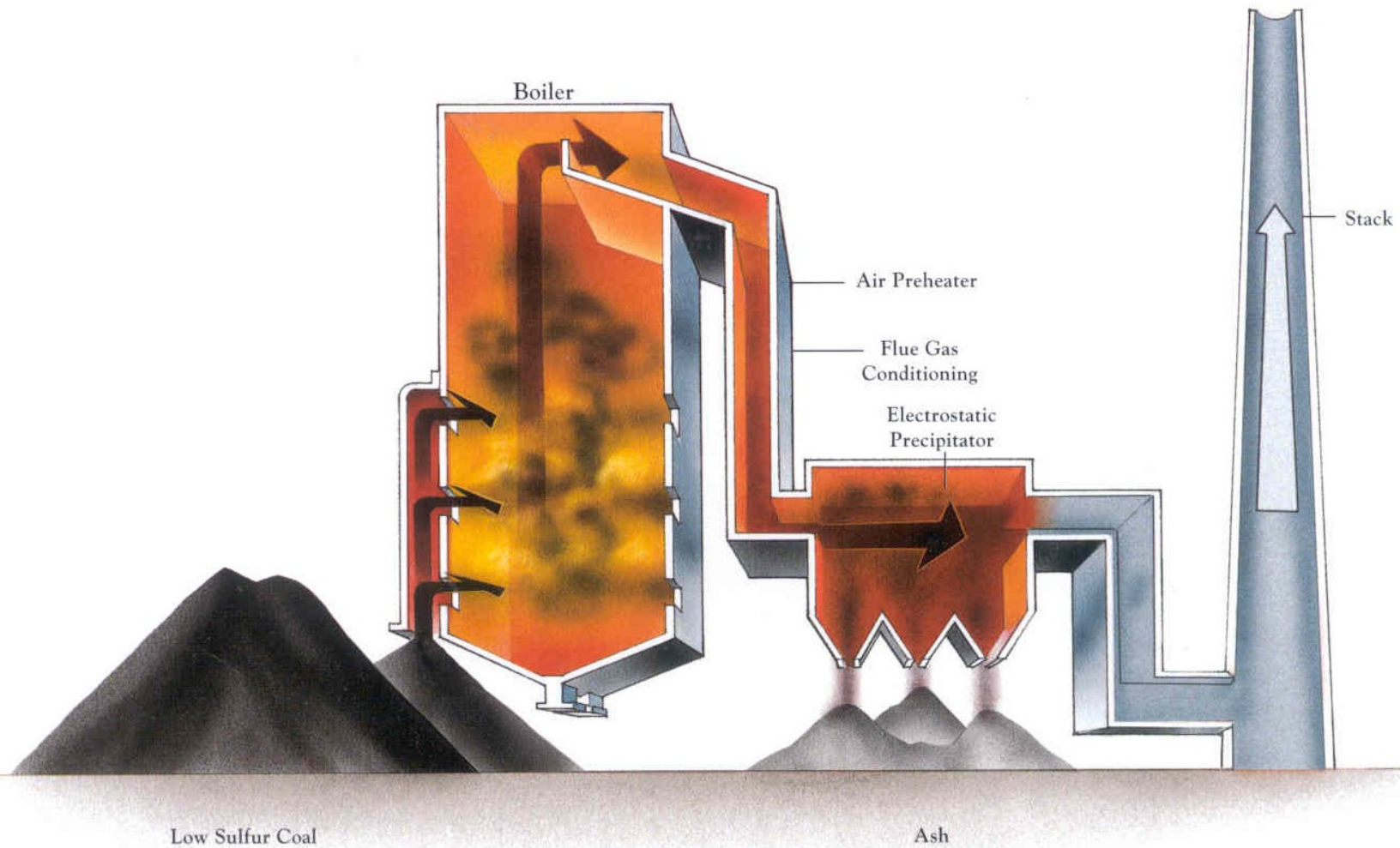


Sulfur Trioxide

- Toxic highly reactive gas
- Combines with water vapor to form sulfuric acid mist
- Gas above 500 deg F
- Generally produced by burning sulfur and catalytic oxidation of Sulfur Dioxide gas
- Typical inject 5 to 15 ppm in Flue Gas ~ 20 to 300 lb/hr sulfur - 50 to 800 mW



Flue Gas Conditioning Basics



ESP Principles

- Charge the Particles
- Migration of Charged Particles to Collecting Plates
- Move the Collected Material to the Hopper for Removal



Dust Layer on Plates

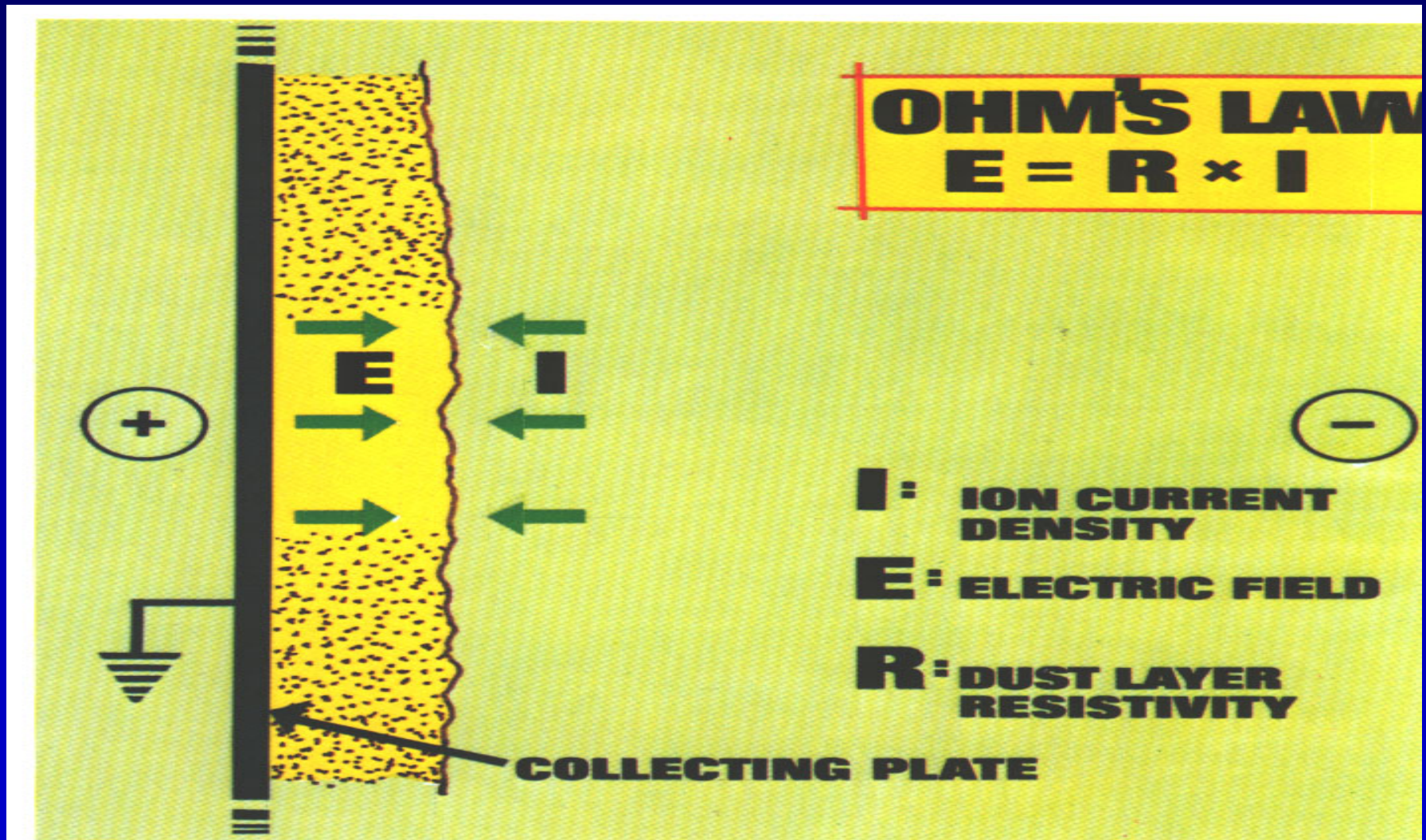
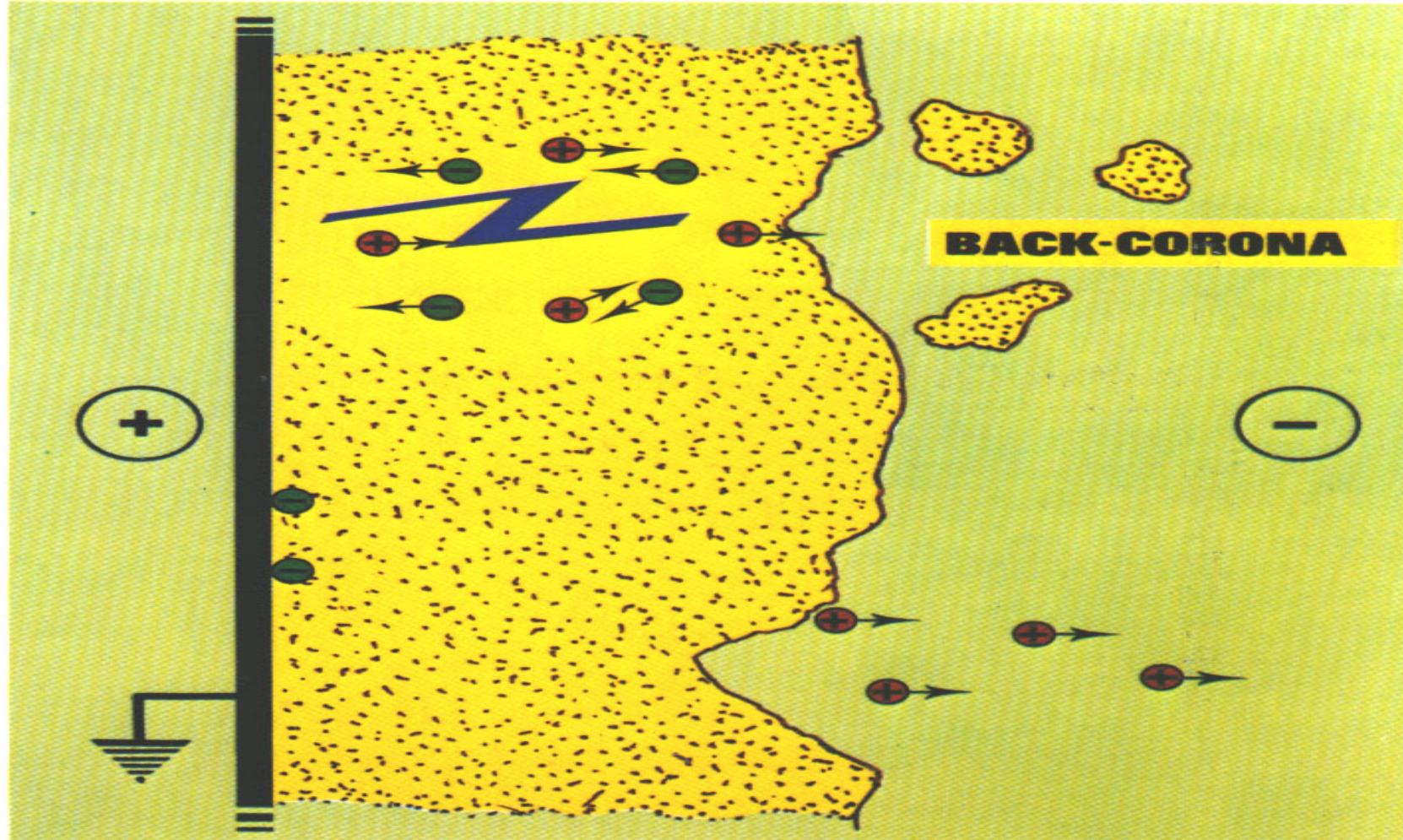


Fig 8: The electric field in the dust layer

High Resistivity Dust Layer

Fig 9: Back-corona in the dust layer



VI Curves - Normal

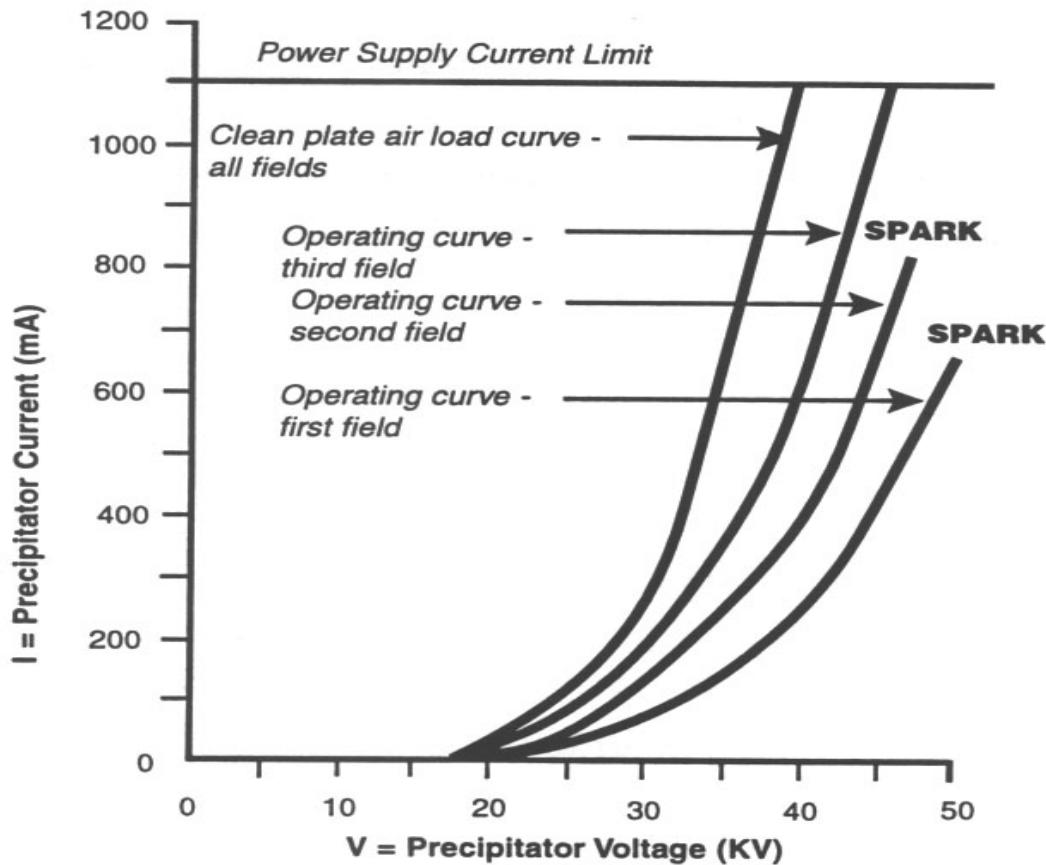


Figure 4.13
Normal Precipitator Voltage-
Current (V-I) Curves



VI Curves – High Resistivity

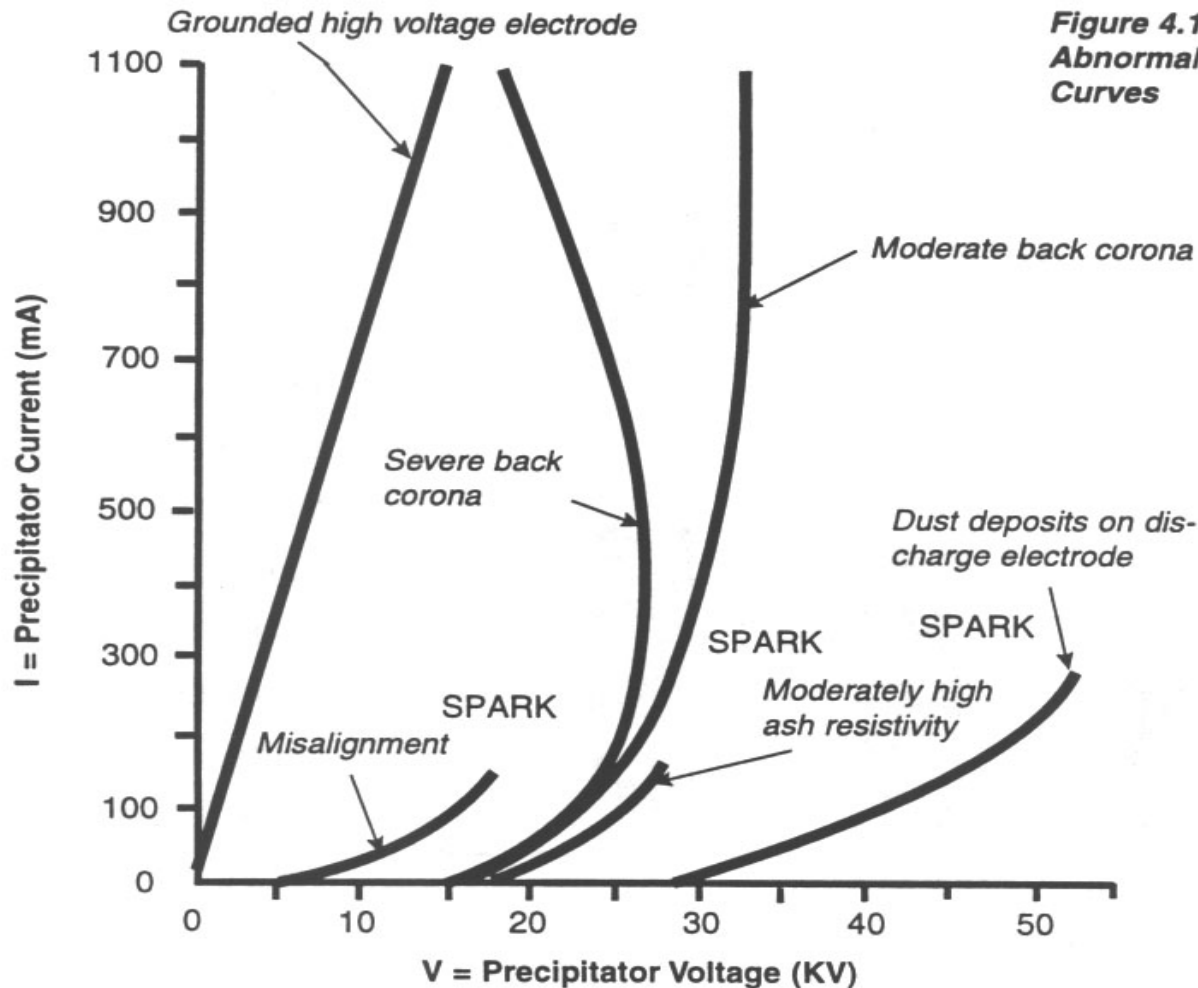
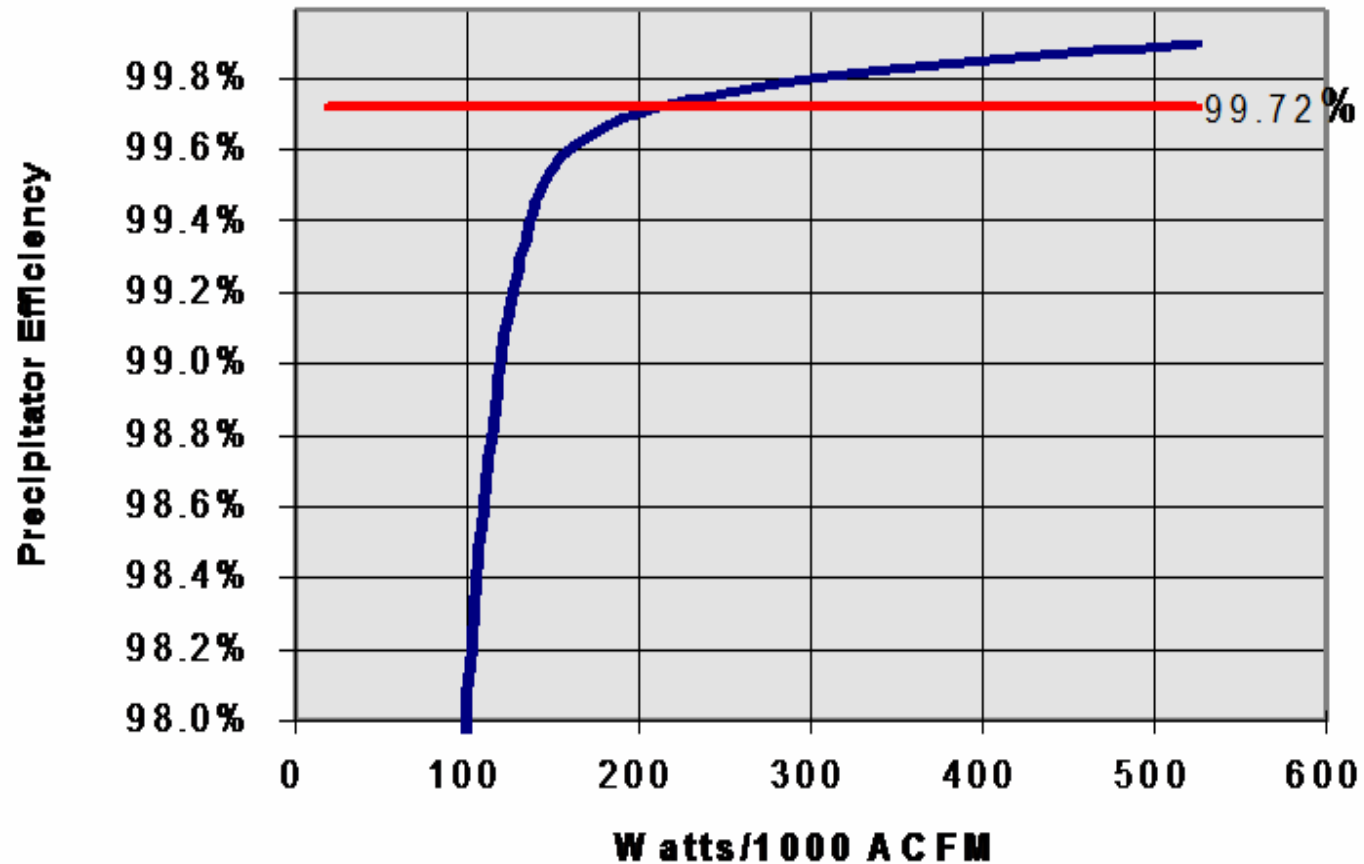


Figure 4.14
Abnormal Precipitator V-I
Curves

Precipitator Efficiency vs. Power

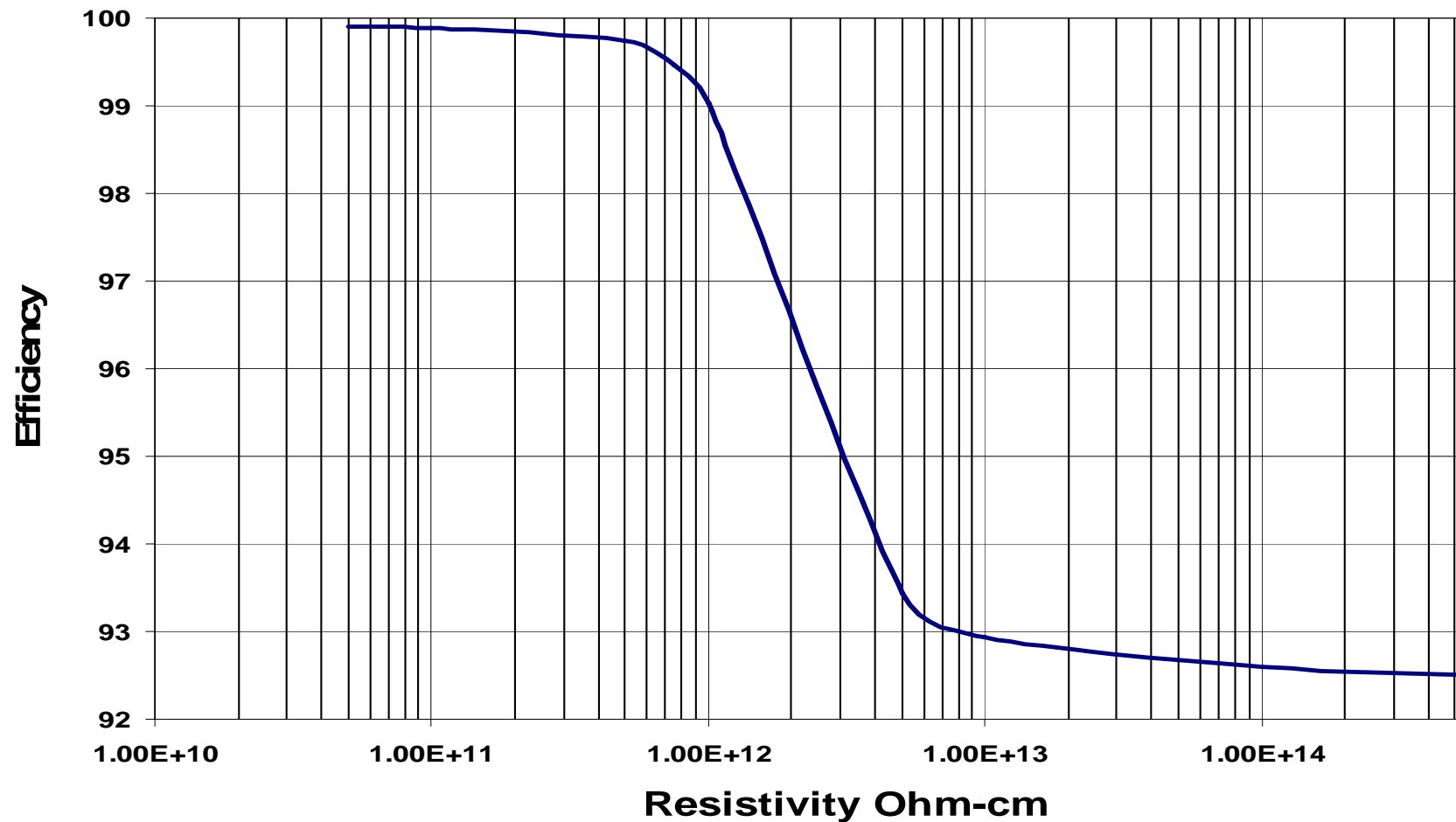


EPRI CS2908



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ESP Efficiency vs. Resistivity for SCA 325 ft²/1000 acfm



Sulfur Trioxide FGC

- SO₃ Reacts with moisture in flue gas
- Absorbed on surface of fly ash
- Improves surface conductance of ash
- Lowers the surface resistivity

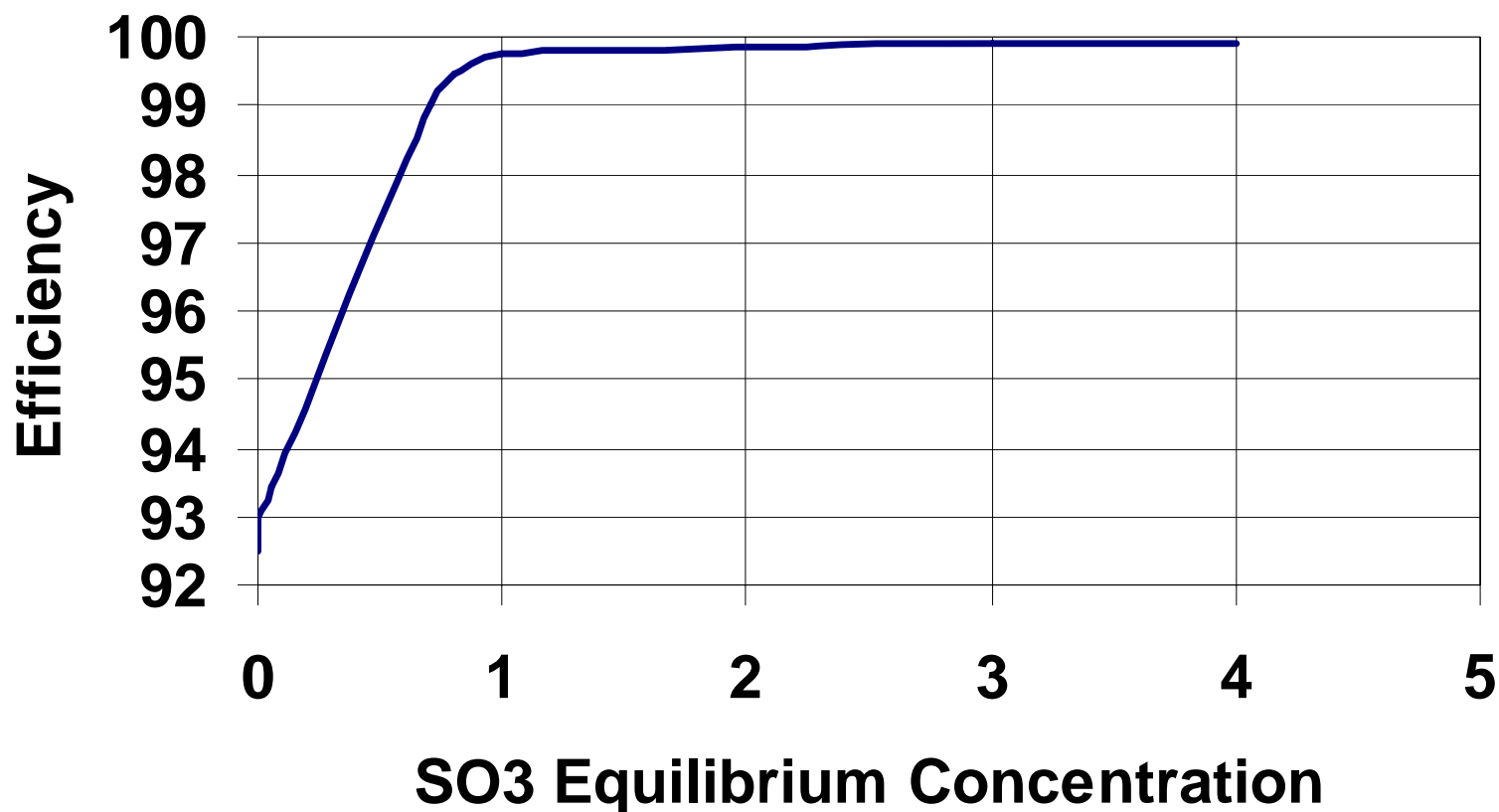


Ash Resistivity

- Surface Conduction
- Volume Conduction
- Optimum is between
 - 1×10^8 ohm- cm
 - And
 - 1×10^{10} ohm – cm
- Ash measured in Laboratory in Oven and High voltage Cell
- Computer model developed based on Ash Analysis



Precipitator Efficiency vs. SO_3 for ESP of 325 SCA



Resistivity Model

- Laboratory measurement developed by WP
- Dr Bickelhaupt SRI developed mathematical model
- Based on Ash and Coal Chemistry



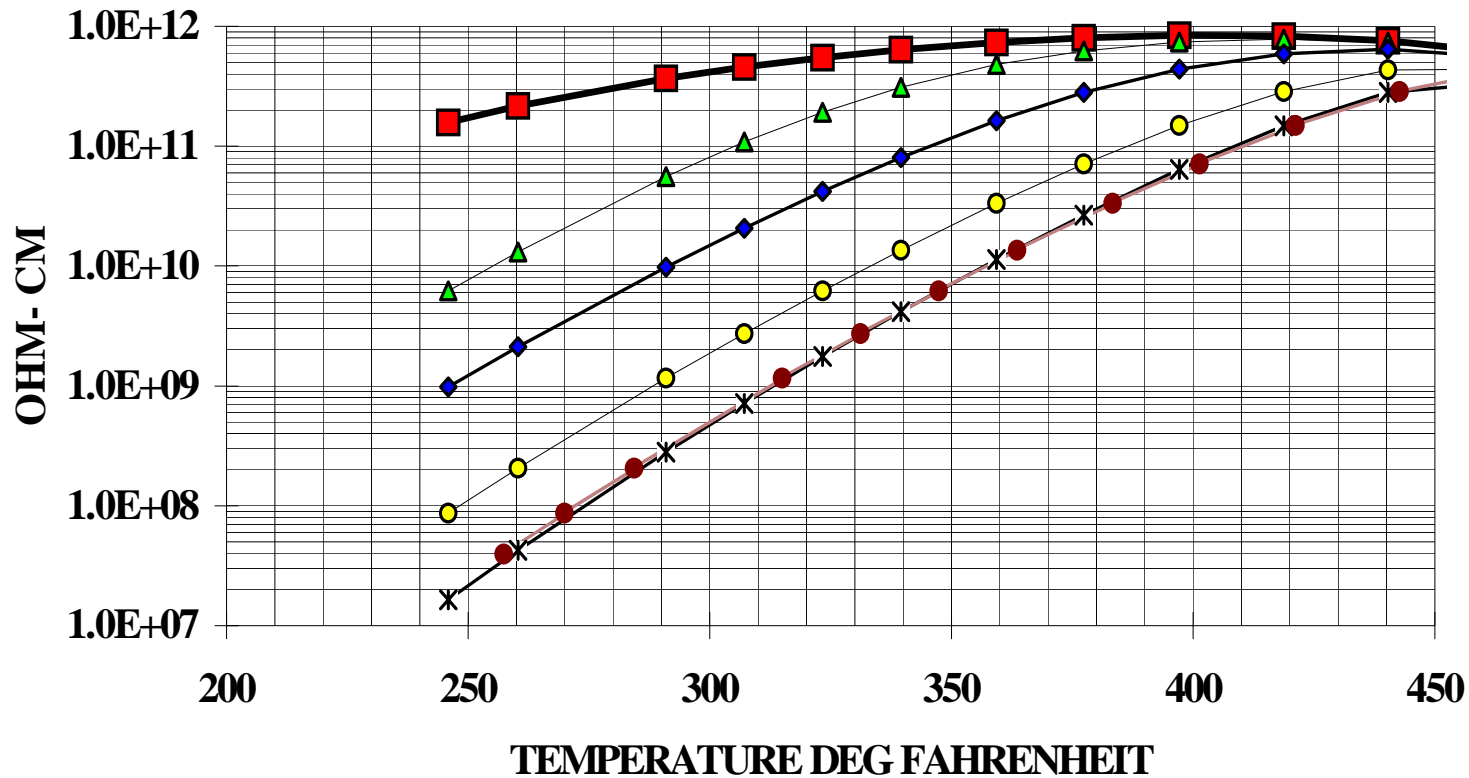
PRB

TVA -- Johnsonville
PRB -- Average

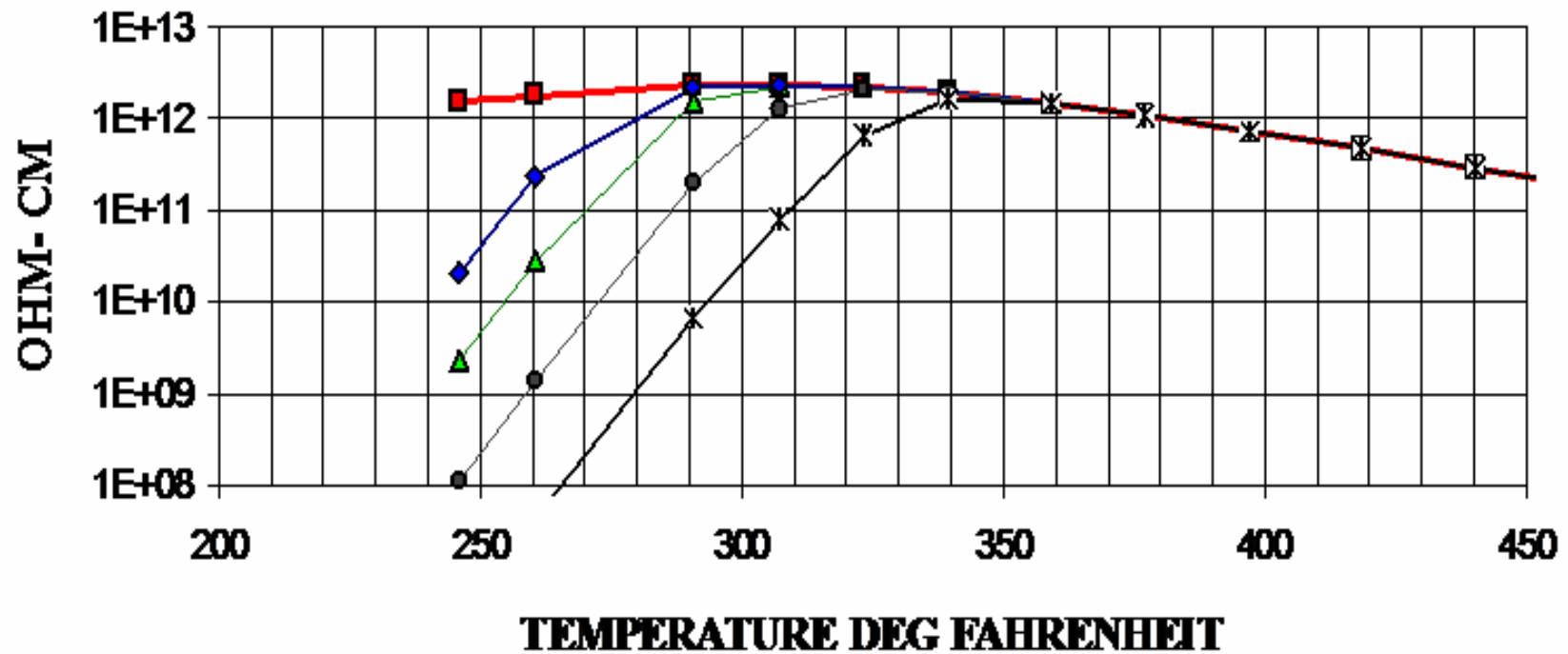
EXPECTED RESISTIVITY

Ash Spectrographic
Analysis

Li2O=
K2O=1.
CaO=
Al2O3=1
TiO2=1.
SO3=20.
Na2O=0.
MgO=3.
Fe2O3=7
SiO2=28
P2O5=0.



Low Alkali



■ No SO3 ▲ Predicted Coal SO3 ◆ 1 PPM SO3 ● 4 PPM SO3 × 10 PPM SO3

Dual Conditioning

- Inject both SO₃ and Ammonia independently
- Ammonia improves attachment of SO₃
- Extend performance at higher temperatures
- Reduces precipitator ash reentrainment



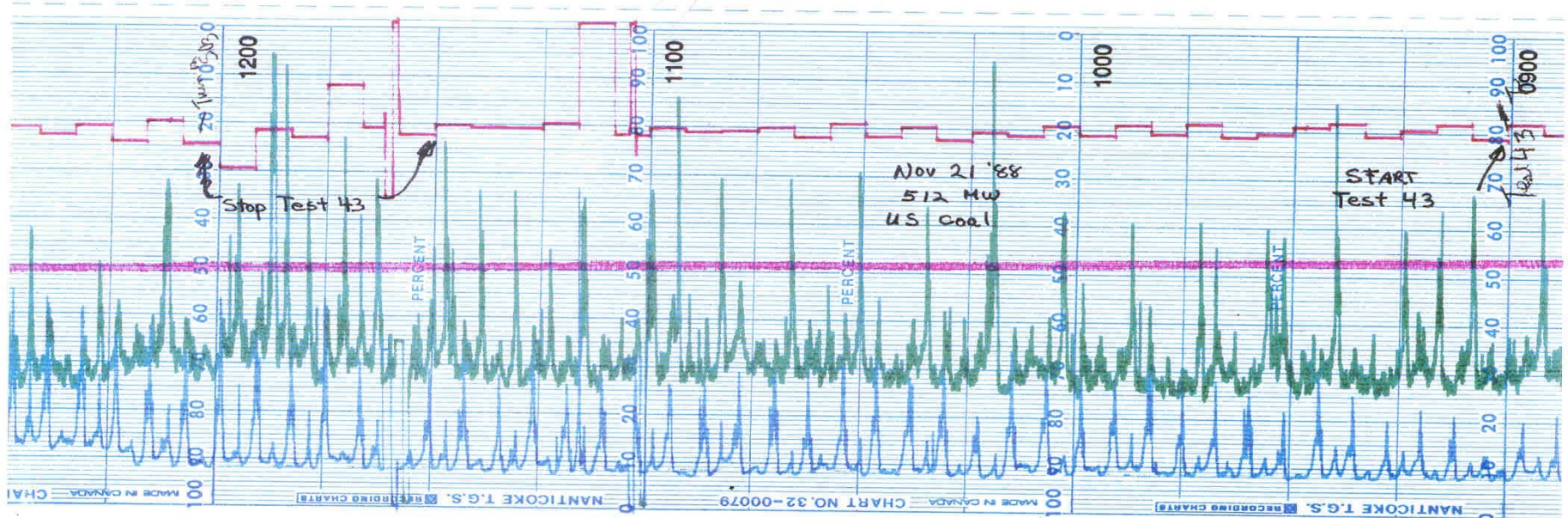
Nanticoke Dual FGC Results

- SO3 – Opacity reduced from 22 to 15%
- With Dual FGC opacity 8%
- Substantial increase in Particle Size
- Dramatic reduction in rapper spikes
- Reduction in opacity baseline
- No hopper ash removal problems encountered



Nanticoke No FGC

NANTICOKE UNIT 2 OPACITY

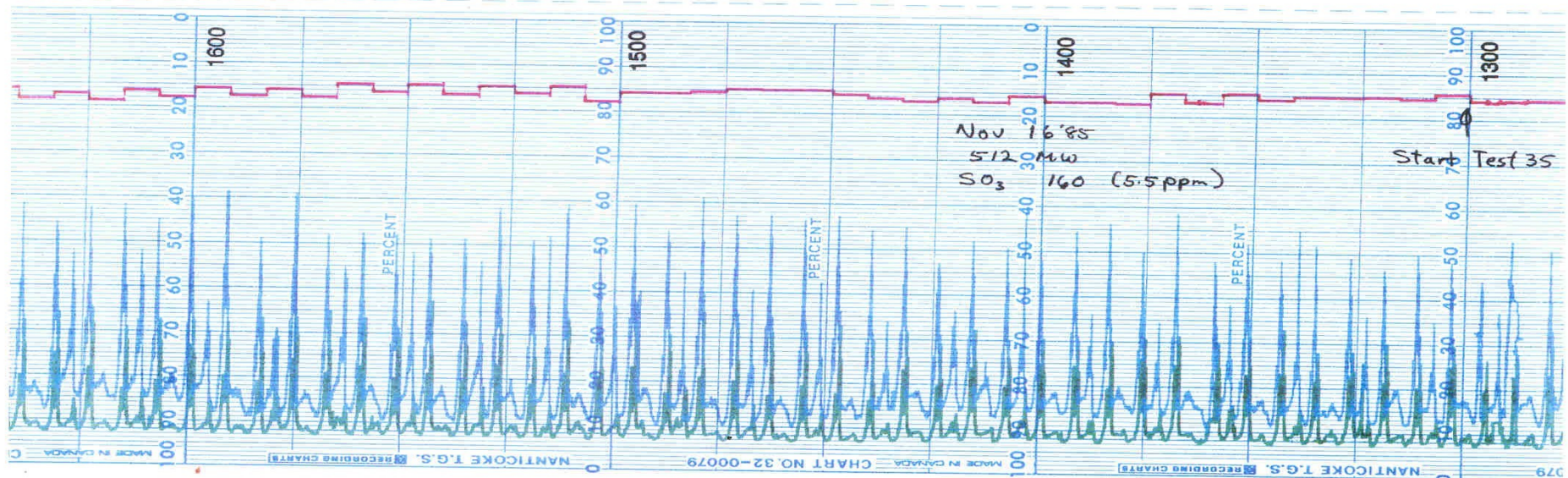


LOW SULFUR 50/50
TEST 43
SO3 OFF
NH3 OFF



Nanticoke SO3 Only

NANTICOKE UNIT 2 OPACITY

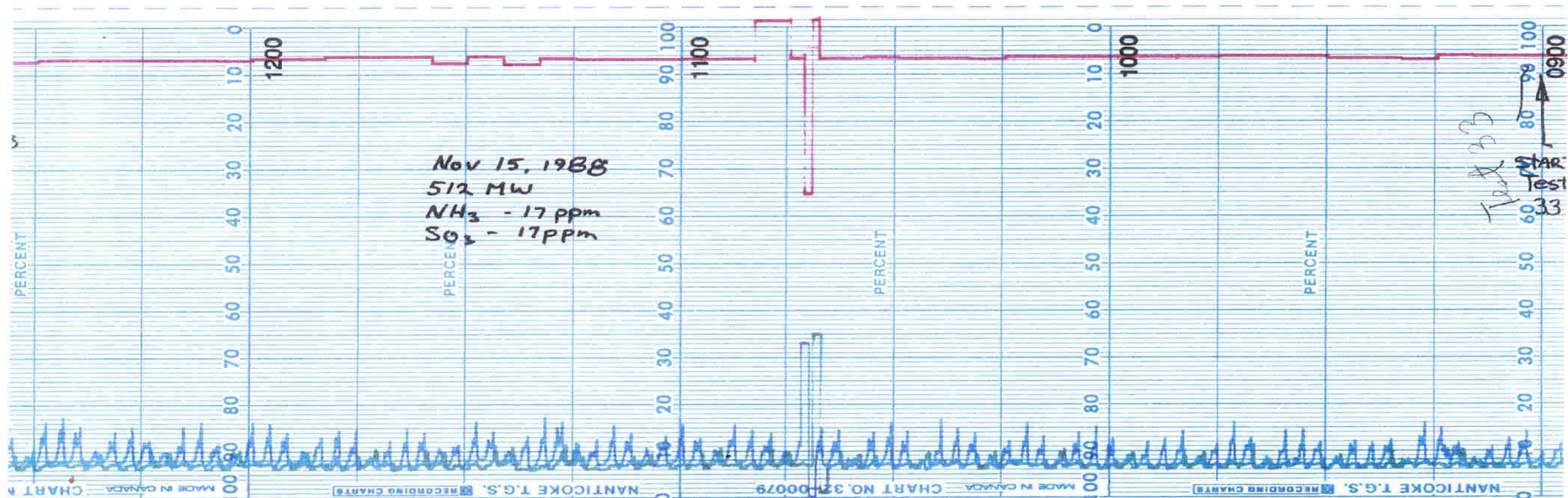


LOW SULFUR 50/50
TEST 35
SO₃ 5.5 ppm
NH₃ OFF



Nanticoke Dual FGC

NANTICOKE UNIT 2 OPACITY



LOW SULFUR 50/50
TEST 33
SO₂ 17 ppm
NH₃ 17 ppm



Equipment Design Issues



Critical Design Principles

- Injection into Flue Gas
 - Must remain above Dew Point
 - Piping Heat Loss Issues
 - Energy Consumption
 - Proper Distribution
- SO₃ Converter Inlet Temperature
 - Conversion Efficiency
 - Catalyst Life
- Burner Issues
 - Sulfur Purity
 - Complete Combustion



Injection Location Criteria

- Achieve > 1 second residence time
- Nozzle Spacing $< 1/10^{\text{th}}$ Mixing Distance
- Hot Gas Piping not excessive length
- Accessible Location
- Hot Side / Cold Side



Injector Sizing Principles

- Achieve Uniform Distribution
- Mixing
- Maintain Adequate Injection temperatures
- Maintain Injection velocities



SO₃ Distribution Issues

- Generally strive for uniform concentration
- If SO₃ concentration were varied within a duct what would the parameters be:
 - Gas temperature
 - Velocity
 - Dust Loading Concentration
 - Particle Size

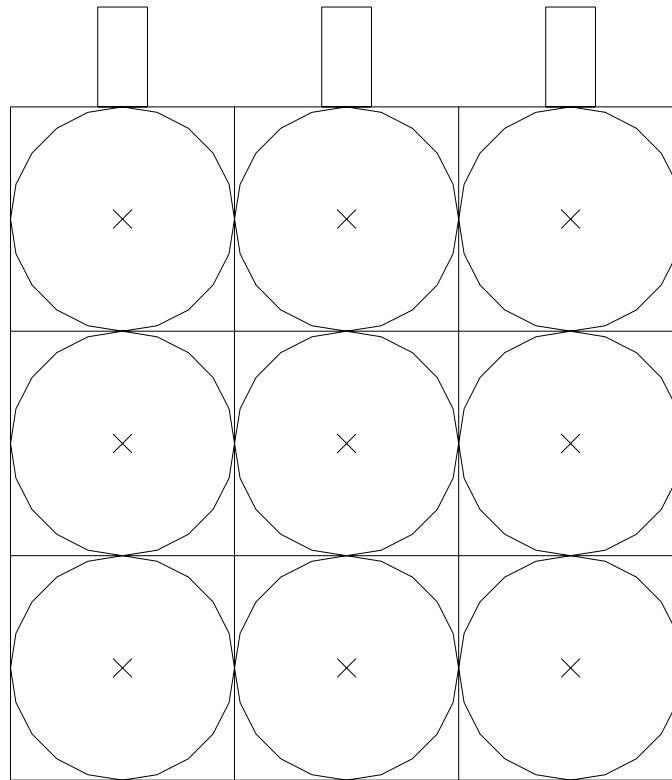


Injector and Nozzle Spacing

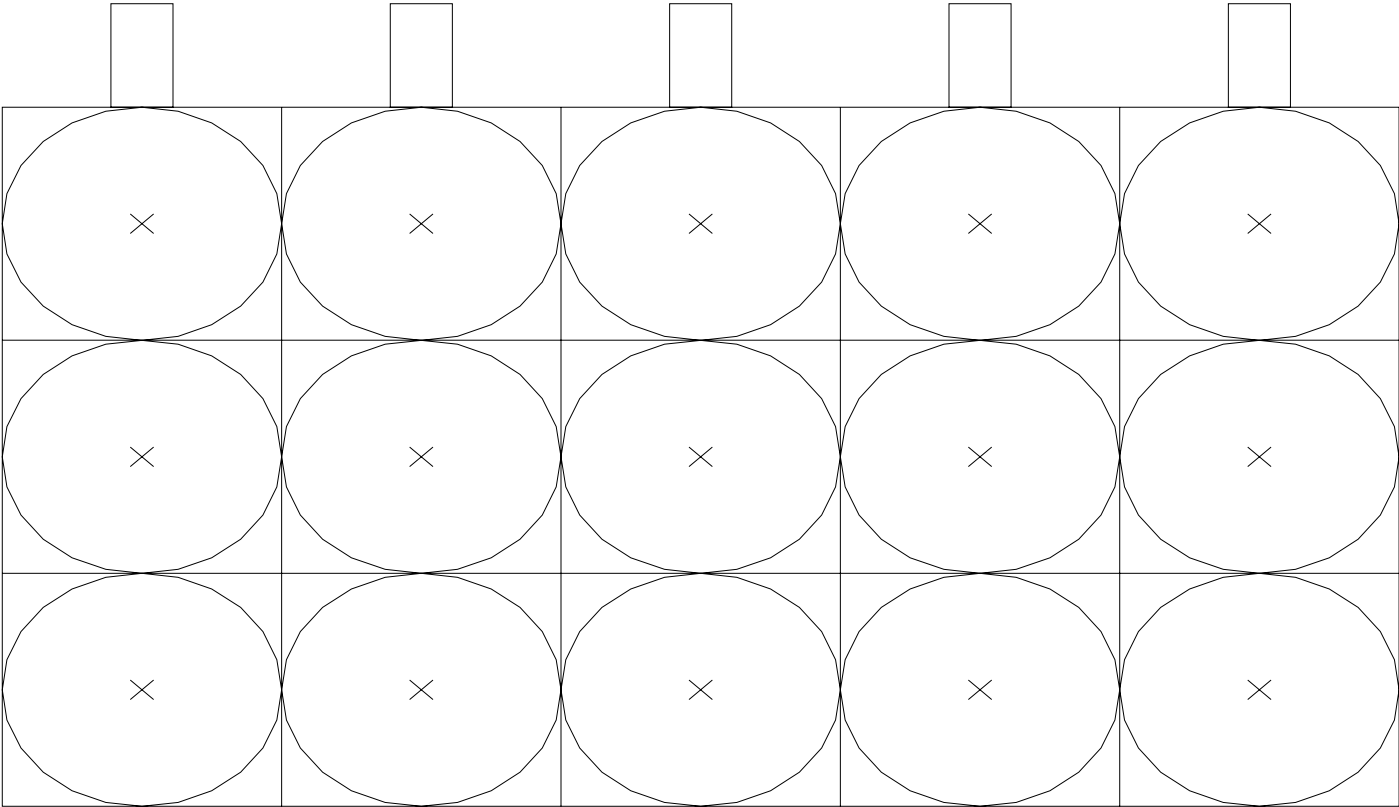
- Inject into Centroid of Square Equal Areas
- Adequate Injection Points
- Minimize Number of Injectors
- Injectors Usually about 3 feet apart



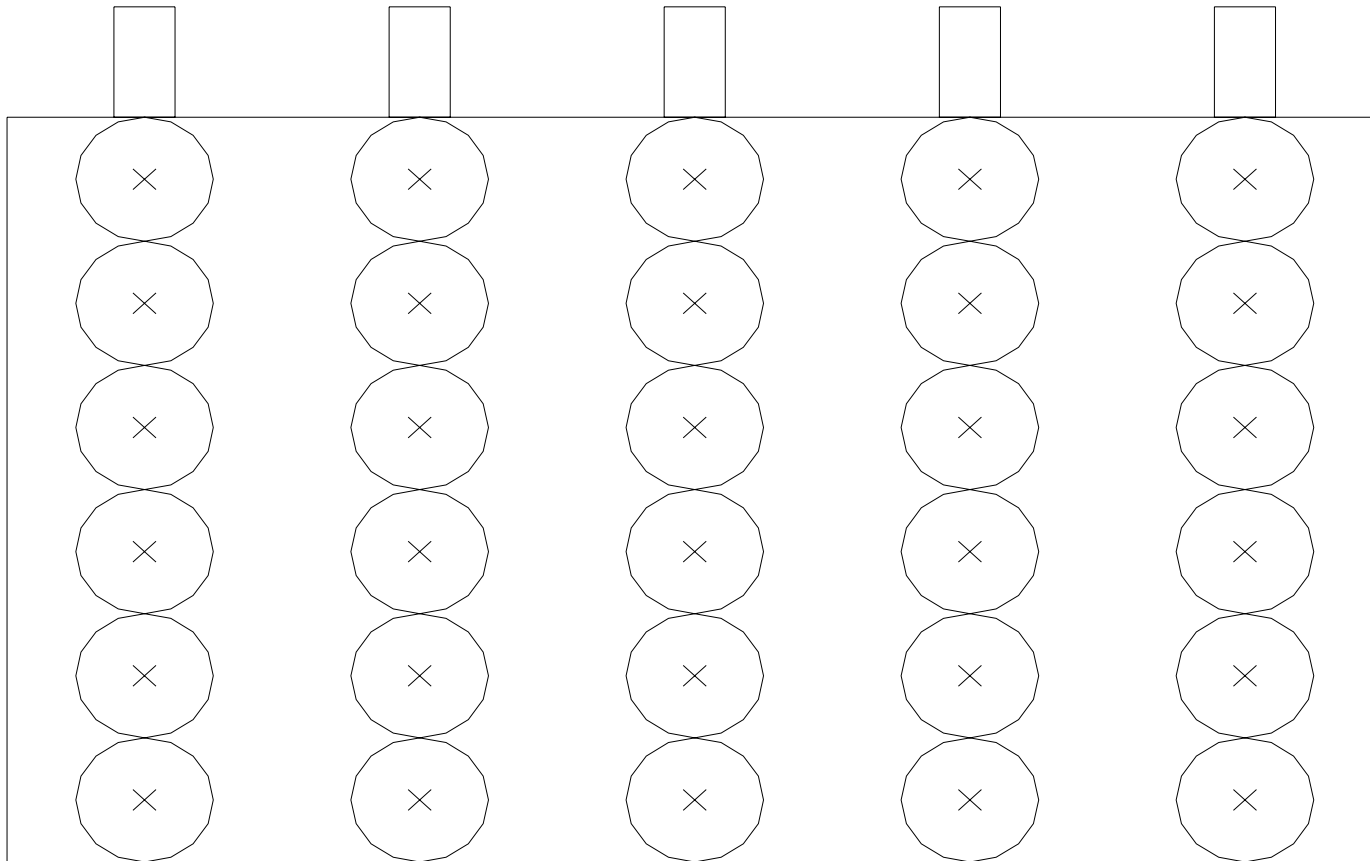
Square Duct Injector Spacing



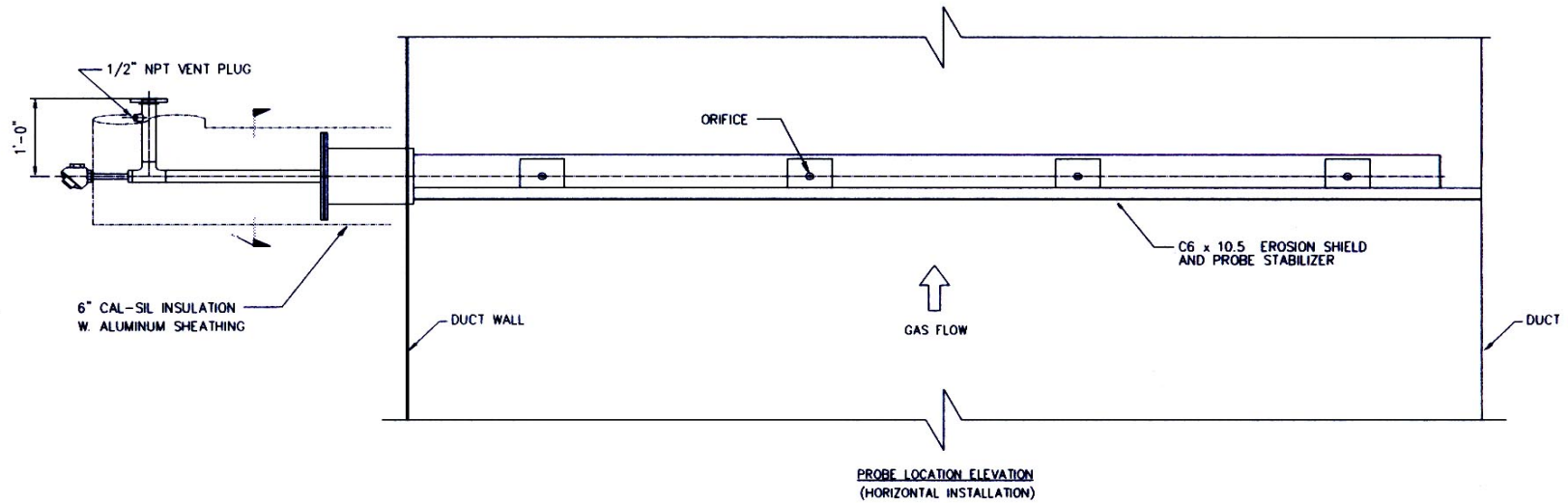
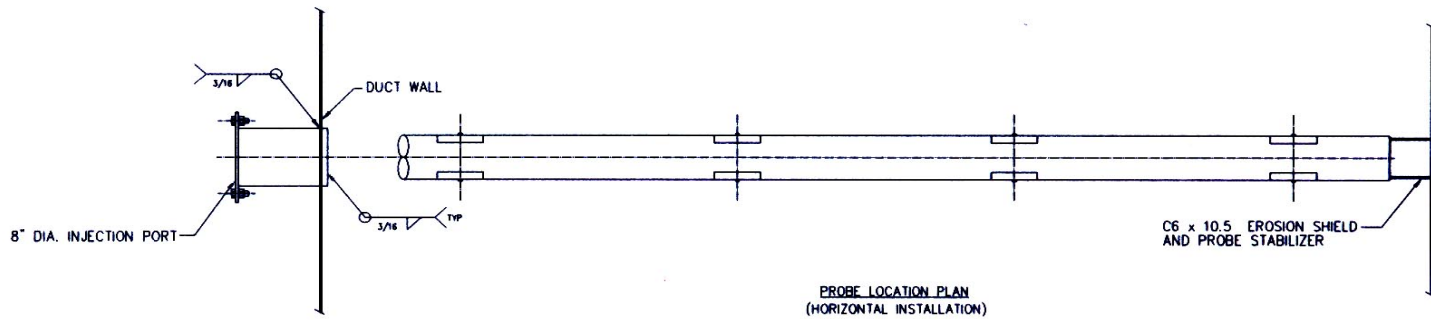
Rectangular Duct Injector Spacing



Improper Nozzle Spacing



Typical 'Old Style' Design

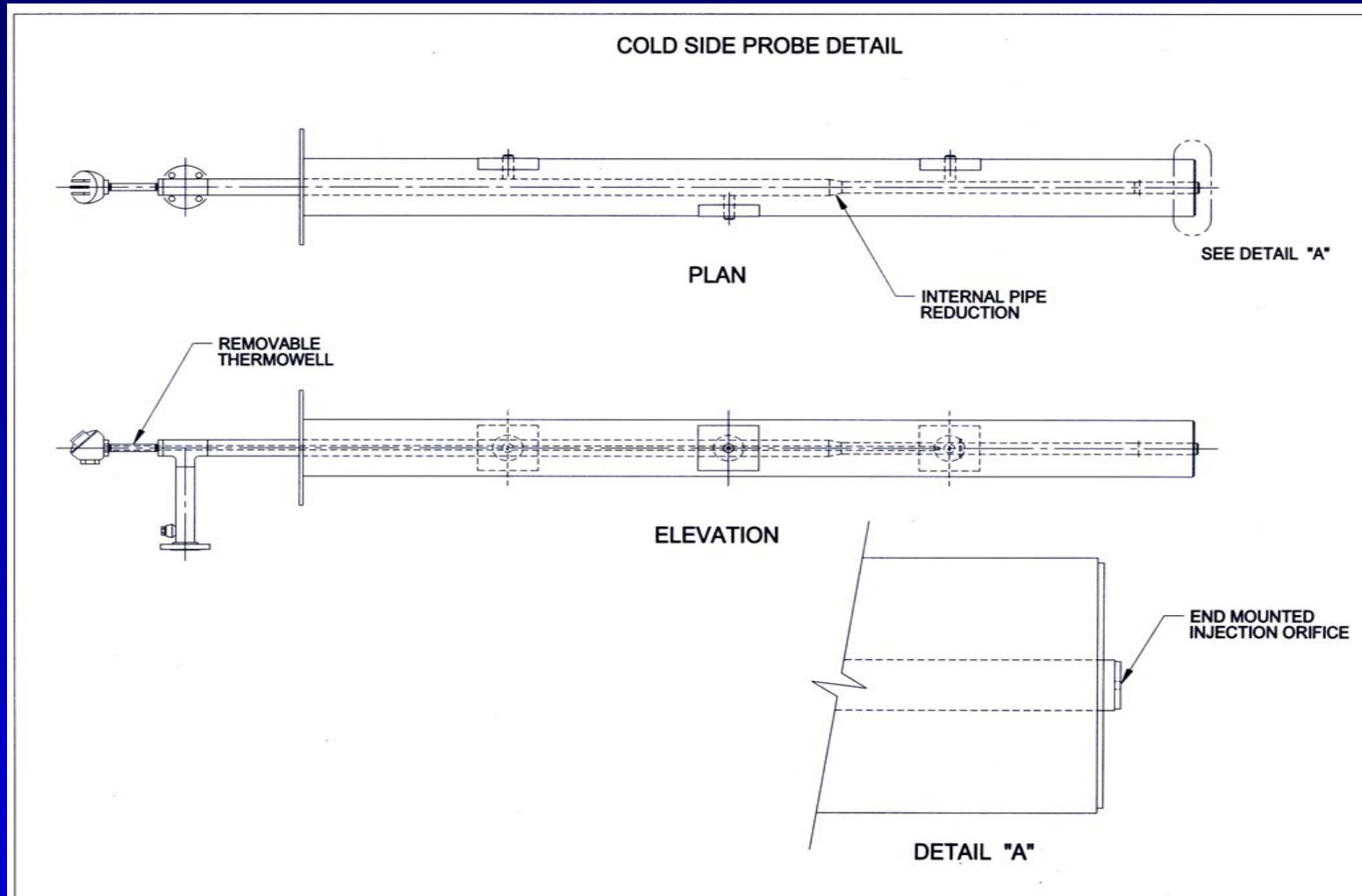


Improvements in Design

- Less nozzles
- Larger nozzles
- Improved Purging
- Nozzle at End of Injector
- Clean Out Path



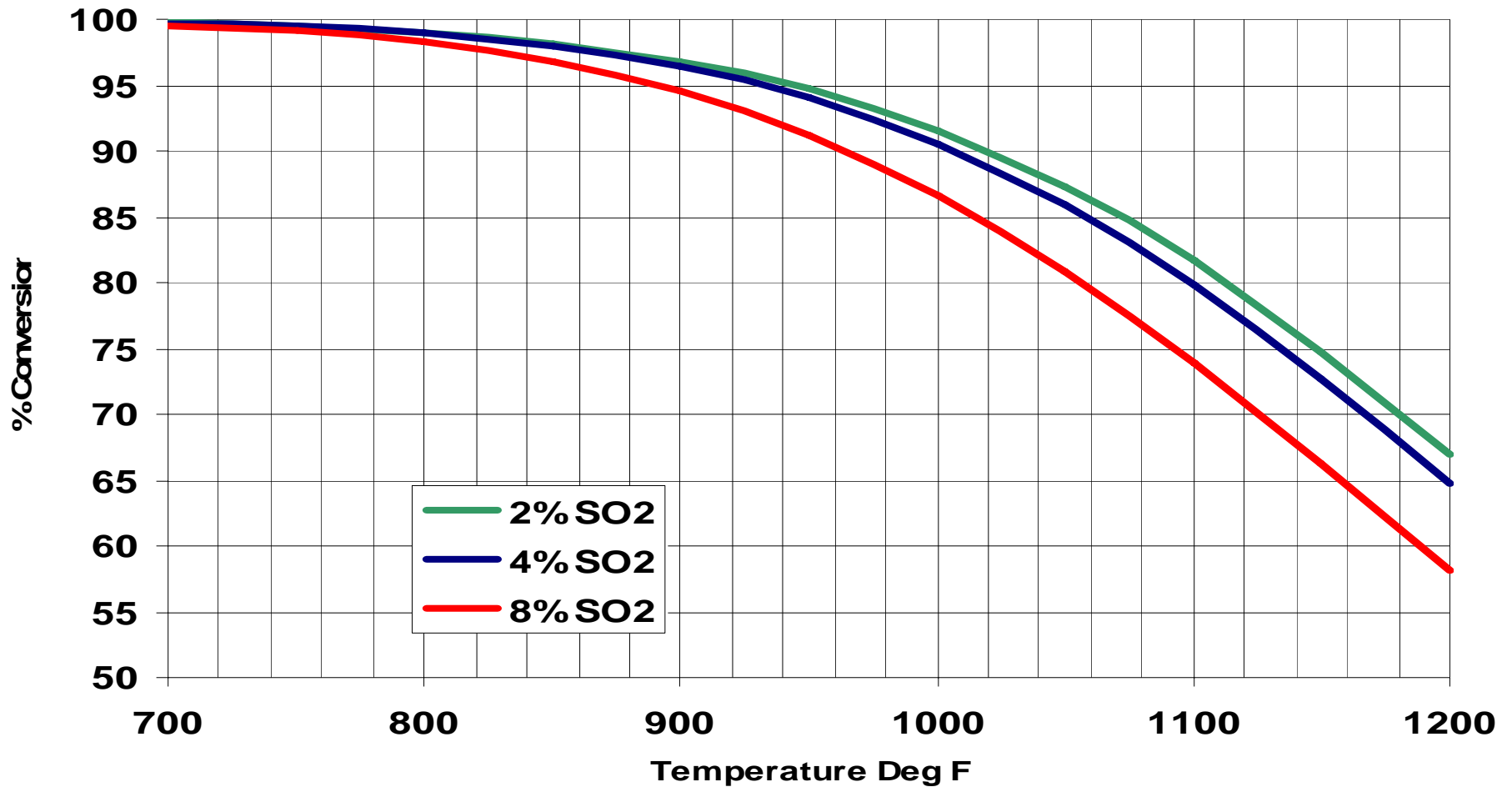
New Design



Design Improvements



Equilibrium Conversion for SO₂ Oxidation



High Efficiency Converter

- Low SO₂ Gas Concentration
 - Improved Equilibrium Conversion
- Design Converter Gas Velocity Low < 3 fps
- High Activity First Catalyst Layer
 - Lower Light off temperature
 - Lower Outlet Temperature
 - Higher Conversion
- Second Layer Conventional Catalyst



SO3 System in Enclosure



Advanced Ring Main Sulfur Pumping System

- Constant speed centrifugal pumps
- Robust low maintenance design, highly reliable, industry standard
- Redundant sulfur pumps
- Sulfur metered with Coriolis Flow Element
- Controlled at each sulfur burner with flow control valve



Air Heater Features

- Over sized air Heaters
- Rapid Startup
- Operating watt density less than design of 20 watts/ sq in
- Small easy to handle modules
- Vertical design assures good air distribution





- Air Heater

11.5.2003



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Hot Side Injection

- Increased SO₃ Residence time
- Minimal Injector Plugging
- Improved SO₃ Distribution
- SO₃ always above dewpoint – no injector corrosion
- Ideal for Tubular Air Heaters

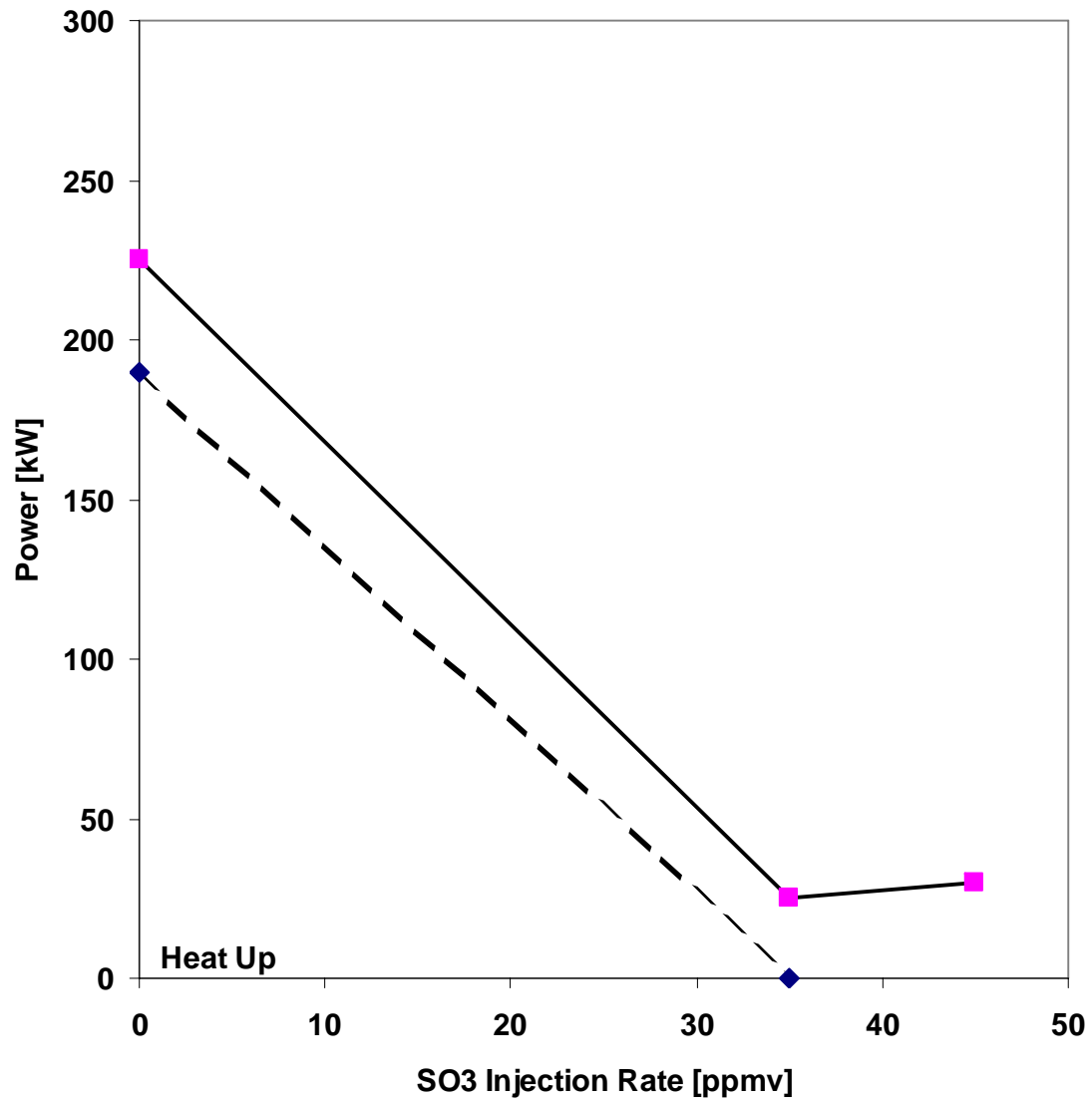


Low Energy Consumption Design

- Significant Energy Savings
- Air Flow Varies with Sulfur Rate
- High Gas Volume for Rapid Startup
- Air Heater off at about 60% of Design



Sulfur Burner 500 MW Injection Rate vs. Power



Advantages of Molten Sulfur Feed

- Molten Sulfur $\frac{1}{5}$ to $\frac{1}{2}$ Cost
- Less Manpower Intensive
 - 20 tons unloaded in half hour
 - No Silo to Maintain
- Lower Energy Consumption
 - Sulfur is delivered molten
- More tolerant of Impurities
 - Large settling capacity of Tank



Advantages of Molten Sulfur Feed

- More tolerant of Impurities
 - Large settling capacity of Tank
- Safer
 - No sulfur dust hazards
- Molten Sulfur Readily Available
- Less Mechanical Equipment
- Hybrid Design has worst of both designs

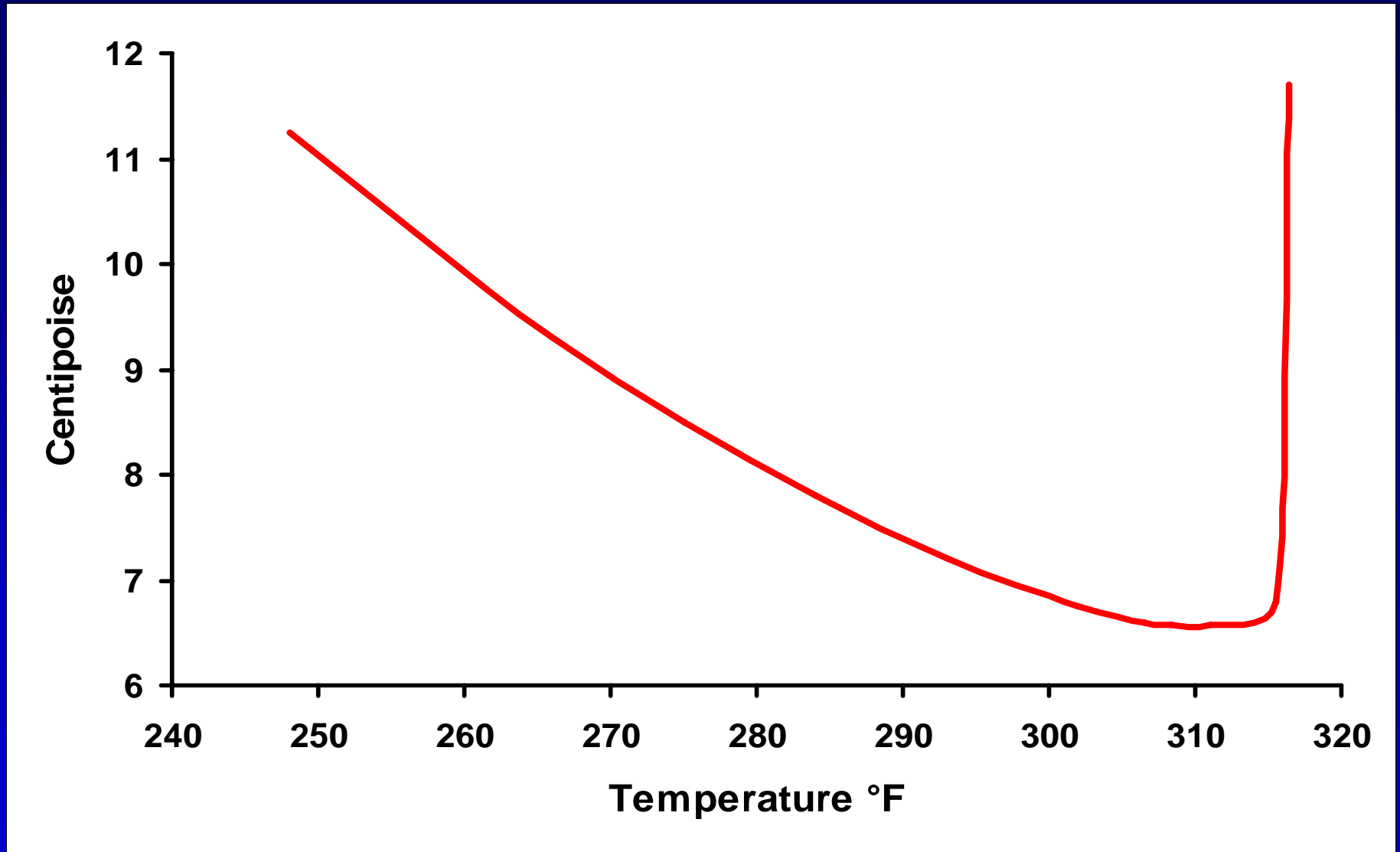


Sulfur Properties

- Heat of Fusion ~ 17 Btu/lb
- Specific Heat 0.16 Btu/lb/deg F
- Molten Sulfur Viscosity of Wide Temperature Range
- 3952 Btu/ lb



Sulfur Viscosity



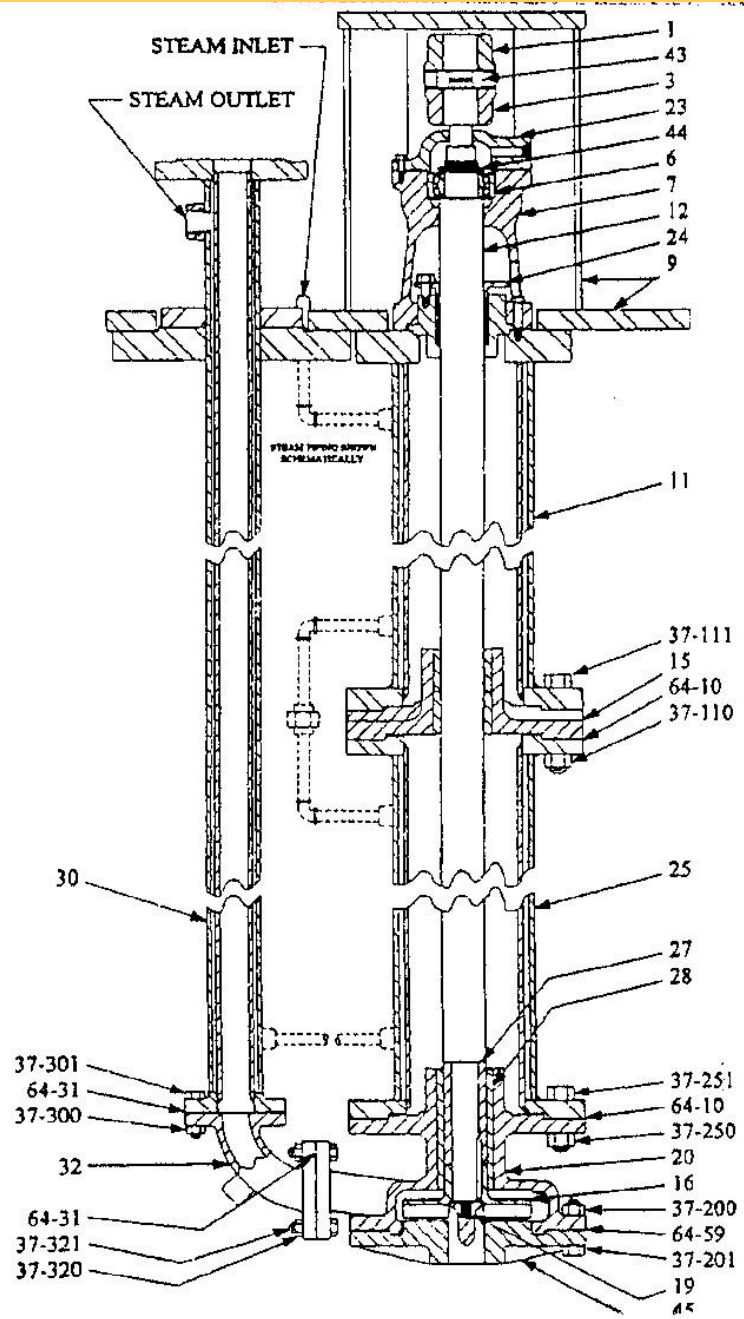
Typical Molten Sulfur Specification

- Sulfur 99.9570%
- Ash 0.0007%
- Organic 0.0036%
- Moisture 0.0872%
- Selenium < 1 ppm
- Tellurium < 1 ppm





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OTHER "J" LENGTHS
AVAILABLE
UPON REQUEST



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Summary

- Approximately 1500 FGC units installed worldwide
- Refined over 30 years
- Many units over 25 years still operating
- New systems use only 10% of the energy of older system
- Application of the technology is predictable
- Successful and competitive ash resistivity correction



Questions

